

(12) UK Patent Application (19) GB (11) 2 271 236 (13) A

(43) Date of A Publication 06.04.1994

(21) Application No 9319754.9

(22) Date of Filing 24.09.1993

(30) Priority Data

(31) 04279158 (32) 25.09.1992 (33) JP

(71) Applicant(s)

Kokusai Denshin Denwa Kabushiki Kaisha

(Incorporated in Japan)

2-3-2 Nishishinjuku, Shinjuku-ku, Tokyo-to, Japan

(72) Inventor(s)

Hidenori Taga

Masatoshi Susuki

Shu Yamamoto

Noboru Edagawa

Hiroharu Wakabayashi

(74) Agent and/or Address for Service

Elkington and Fife

Prospect House, 8 Pembroke Road, SEVENOAKS,

Kent, TN13 1XR, United Kingdom

(51) INT CL⁵

H04B 10/18

(52) UK CL (Edition M)

H4B BK18

(56) Documents Cited

GB 2064161 A EP 0554714 A1 US 5185827 A

(58) Field of Search

UK CL (Edition L) H4B BK18

INT CL⁵ H04B 10/18

Best Available Copy

(54) Optical communication system

(57) An optical transmission system is disclosed, in which the transmission of the optical soliton pulses is controlled by controlling the wavelength dispersion of the optical fiber transmission line for each long section including a plurality of optical amplifier repeaters. In this case, the first sections having an average value of the wavelength dispersion larger than the dispersion value meeting with the soliton condition and the second sections having an average value of the wavelength dispersion smaller than the dispersion value meeting with the soliton condition are alternatively allocated in the optical fiber transmission line, so that the average value of the wavelength dispersion of the entire length of the optical fiber transmission line assumes a positive value.

Digital information is transmitted using return-to-zero modulation.

Fig.2

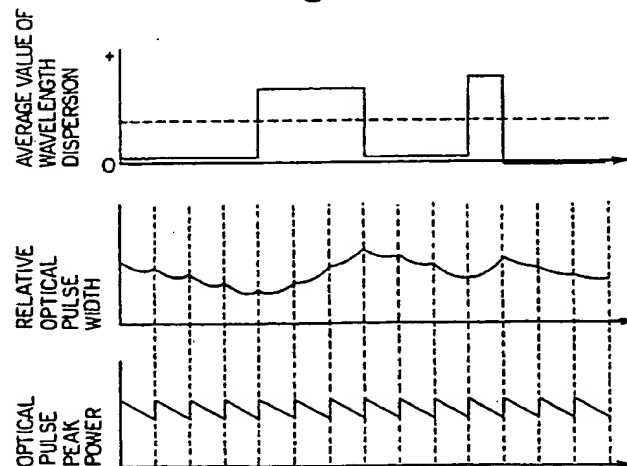
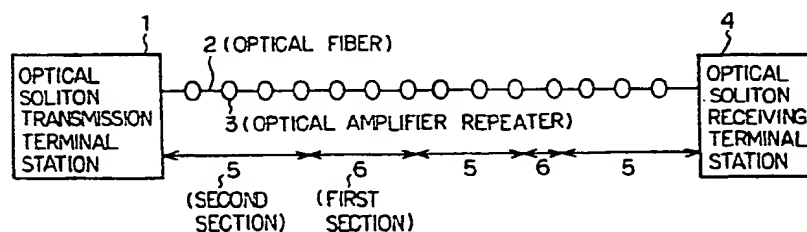


Fig.1



GB 2 271 236 A

Fig.1

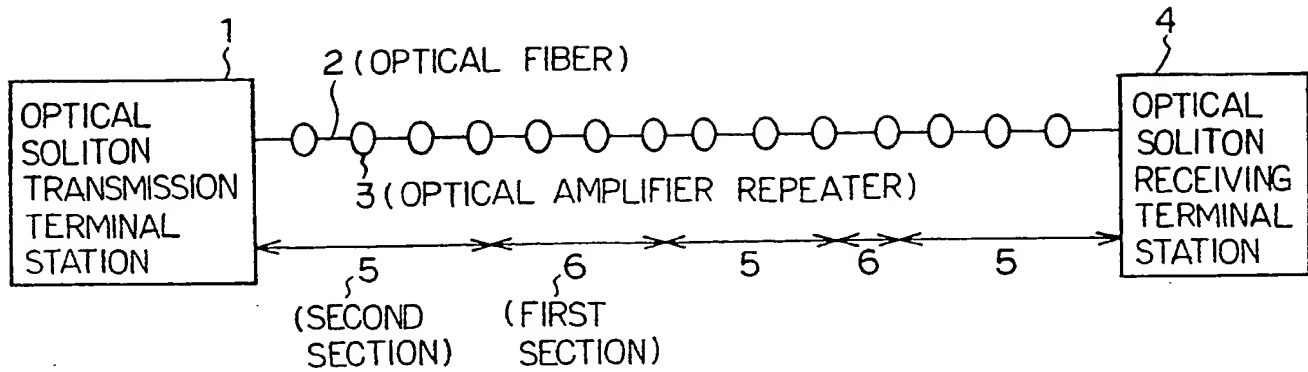


Fig.2

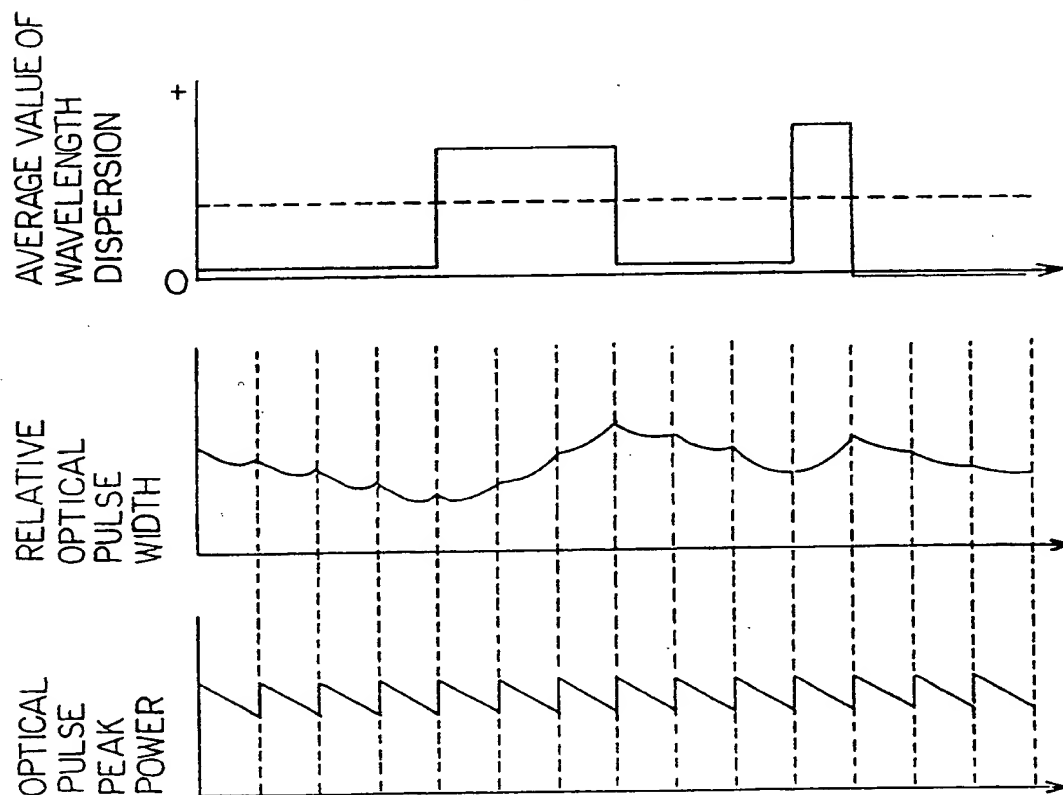


Fig.3A

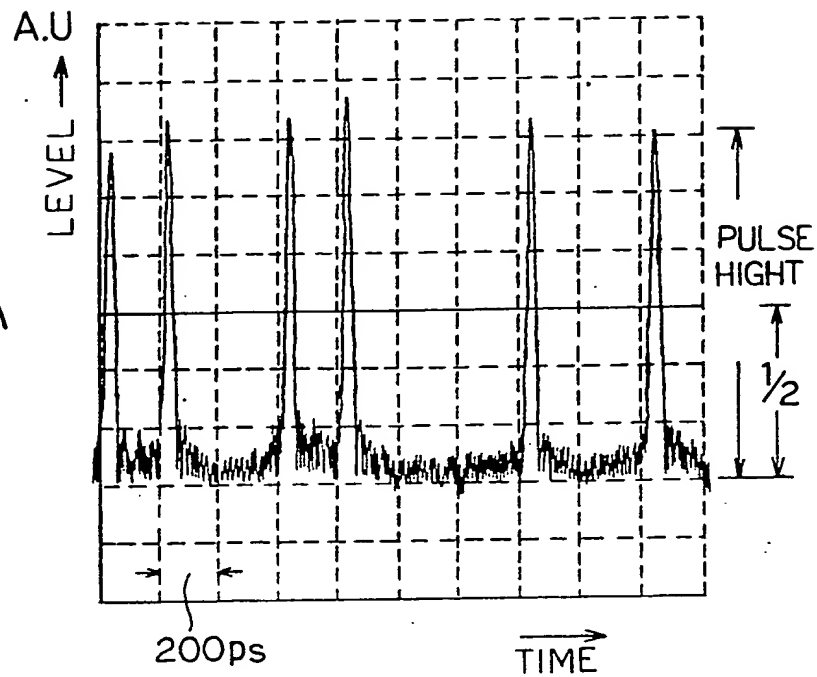


Fig.3B

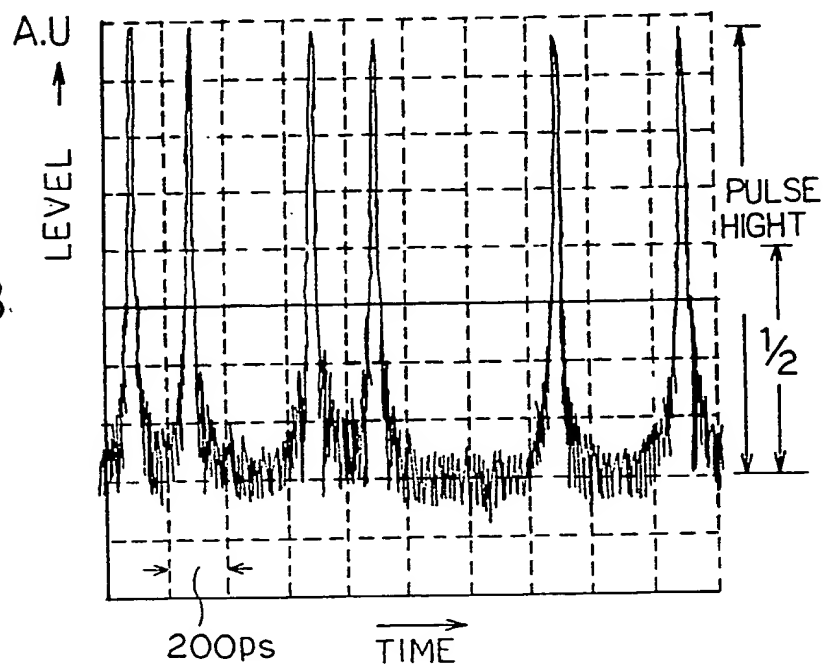


Fig. 4

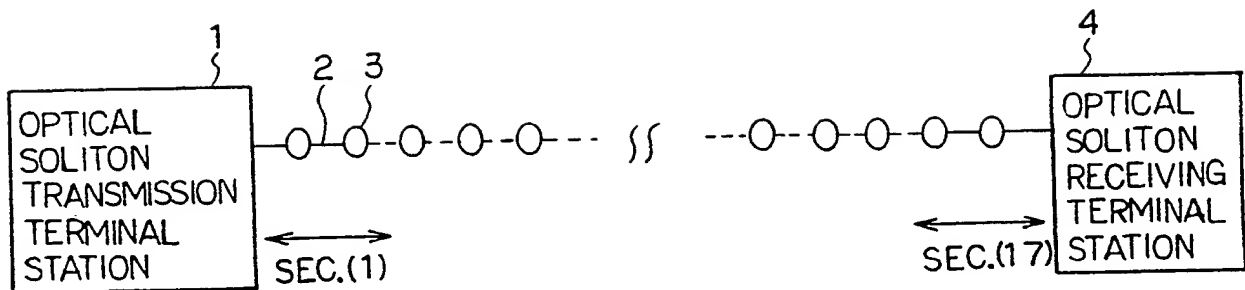


Fig. 5

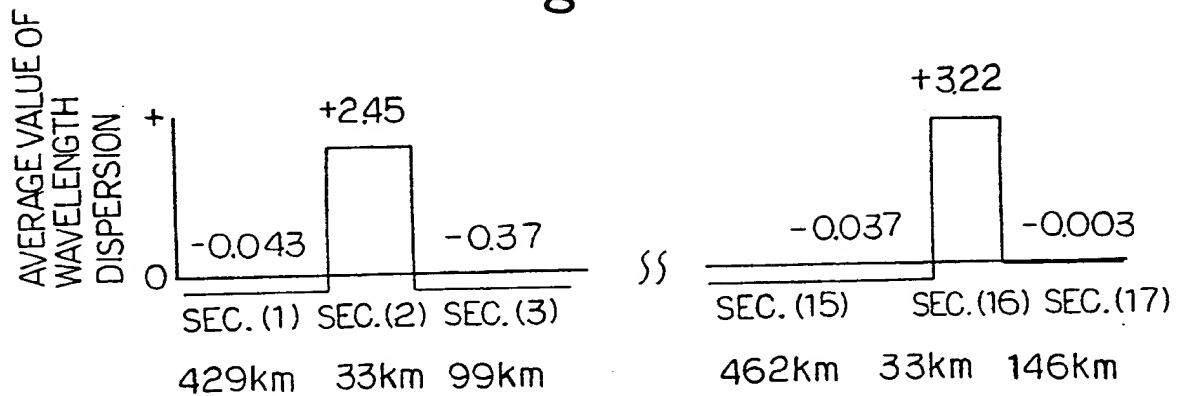
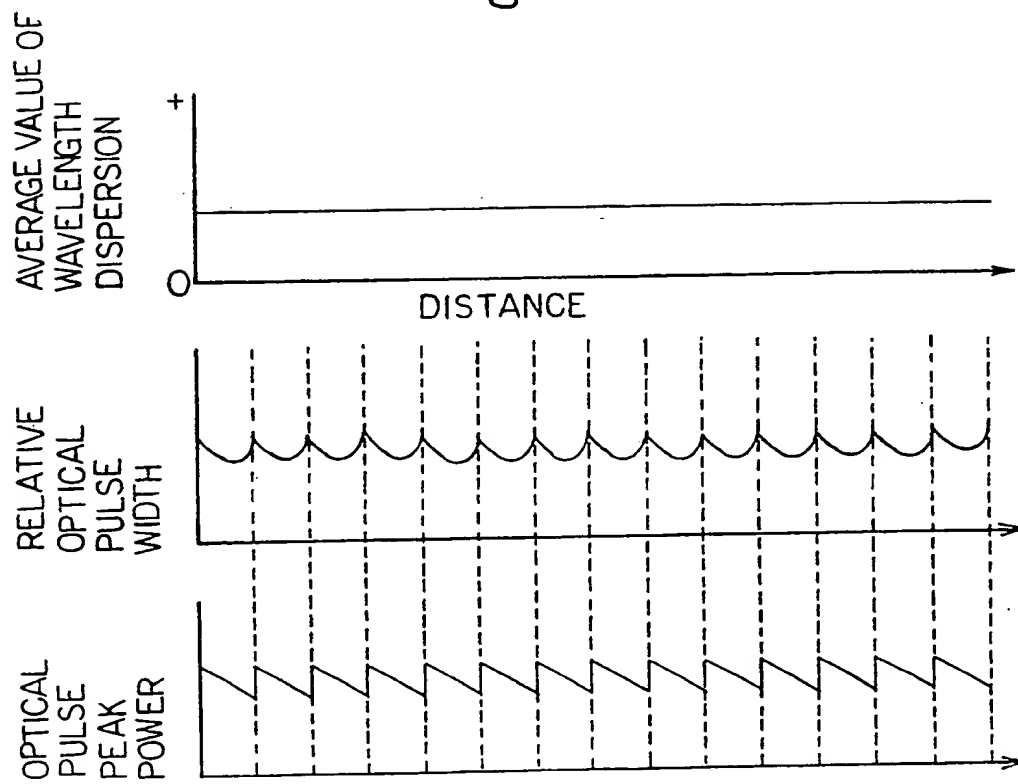


Fig.6



OPTICAL COMMUNICATION SYSTEM

The present invention relates to transmission systems using optical fibers, and more particularly, to an optical communication system including a plurality of optical amplifiers for transmitting optical soliton pulses.

5 In optical fiber communication technique, ultra-long distance systems are now developing on the base of a high-pace progress of the optical amplification technique, so that an optical transmission system over the Pacific Ocean can be realized without using any regenerative repeater. However, communication speed and capacity of the conventional optical communication system are limited
10 since the transmission performance is degraded due to the wavelength dispersion characteristic and the nonlinear optical effect, as the communication speed becomes high. An optical soliton communication system has been closed up as a system capable of eliminating the limitation caused by the wavelength dispersion characteristic and the nonlinear optical effect. This optical
15 soliton communication system is positively using the wavelength dispersion characteristic and the nonlinear optical effect, which are factors of the degradation of the transmission characteristic. The optical soliton pulses can be transmitted without deformation of the pulse shapes since the expansion of the pulse width due to the wavelength dispersion of the fiber is balanced with
20 the reduction of the pulse width due to the nonlinear effect of the fiber. The optical communication system using such optical soliton pulses are now researched to realize a useful communication system because of many advantages, such as capability of large capacity, easiness of multiplexing and no additional deterioration by the nonlinearity of the optical fiber in comparison with a conventional
25 optical communication system. In order to realize an ideal operation of the optical soliton pulses, it is essential that the optical fiber has no loss and the wavelength dispersion D and the soliton peak power P ... meet with the following equation (See a literature: L.F. Mollenauer et al., Journal of Light-wave Technology, Vol. 9, pp194-197, 1991):

$$P_{sol} = 0.77 \frac{\lambda^3 A_{eff} D}{\pi^2 c n_2 \tau^2} \quad (1)$$

In this Equation (1), λ is the wavelength of the optical signal; A_{eff} the effective area of an optical fiber; c the light speed; n_2 the nonlinear coefficient of the optical fiber; τ the full width of the half maximum of the optical soliton pulse.

An actual optical fiber has the loss. Therefore, even if the peak power of the optical pulse and the wavelength dispersion are mutually balanced at the input end of the optical fiber, the effect of the wavelength dispersion increases as the optical pulse transmits through the optical fiber, because the decrease of the peak power causes the pulse broadening and disables the optical soliton pulse operation.

To compensate for this deterioration, a system called as a dynamic soliton transmission was proposed for a long-distance pulse optical soliton pulse transmission system (See: M. Nakazawa et al, IEEE Journal of Quantum Electronics, Vol.26, pp2095-2102, 1990), in which optical power loss is compensated for by the optical amplifiers and the peak power of the optical pulses at the input end of each optical fiber is reset to a value a little more than the power defined by each Equation (1).

In the dynamic soliton transmission system, the optical pulse width is compressed due to the effect of the nonlinearity of the optical fiber caused by the high peak power of the optical pulses at the initial portion of the optical transmission. However, at the end portion of the optical transmission where the power of the optical pulses are attenuated by the loss of the optical fibers, the pulse width is broadened by the effect of the wavelength dispersion of the optical fiber. To compensate for this pulse broadening, an optical amplifier can be inserted at a position where the pulse width is returned to the initial value so that the optical soliton pulse operation can be maintained in

the optical transmission system. In this case, it is required that a section-average power meets with the condition defined in Equation (1). In Fig. 6, the relationship between the optical pulse width and the optical pulse peak power is described.

- 5 The wavelength dispersion in Equation (1) is defined as an average value in a transmission section, and the section length z_0 is shorter than a length Z_0 defined by the following equation:

$$Z_0 = 0.322 \frac{\pi^2 C}{\lambda^2} \frac{\tau^2}{D} \quad (2)$$

- 10 In this Equation (2), D is an average value of the wavelength dispersion of the optical fiber of the transmission section; λ the wavelength of the optical signal; c the light speed; τ the full width of the half maximum of an optical soliton pulse. A length Z_0 defined by Equation (2) is usually called as "soliton period". If the average value of the wavelength dispersion D of the
15 optical fiber of the transmission section meets with the condition defined in Equation (1) and the section length z_0 is sufficiently shorter than the soliton period Z_0 , then the optical soliton pulse transmission can be performed.

In the dynamic soliton pulse transmission, the peak power of the optical soliton pulse is controlled so as to mutually equalize the pulse widths at the
20 input end and the output end of the optical fiber, which are connected between adjacent two of the optical amplifiers. In this case, the average value of the wavelength dispersion should be maintained for each span of the optical fiber.

However, from the viewpoint of manufacturing deviation of the optical fiber, it is impossible to maintain the average value of the wavelength
25 dispersion for each span of 30 Km to 50 Km in an ultra-long distance optical communication system, such as the Trans-Pacific System.

An object of the present invention is to provide a practical optical communication system in place of the conventional dynamic soliton transmission.

According to the present invention, there is provided
an optical communication system comprising :

an optical transmission terminal station for transmitting return-to-zero
optical pulses including digital information;

5 an optical receiving terminal station for receiving the return-to-zero
optical pulses;

an optical fiber connected across the optical transmission terminal station
and the optical receiving terminal station; and

a plurality of optical amplifier repeaters inserted in the optical
10 fiber for compensating for the loss of the optical fiber transmission line;

said optical fiber and said plurality of optical amplifier repeaters
forming an optical fiber transmission line;

an average value of wavelength dispersion on the entire length of the
optical fiber transmission line being a positive value capable of compensating
15 for the pulse compression effect and the pulse expansion effect on the optical
pulses applied to the optical receiving terminal station;

first sections and second sections being alternately allocated in the
optical fiber transmission line;

each of said first sections having an average value of the wavelength
20 dispersion relatively larger than said average value of the wavelength disper-
sion on the entire length of the optical fiber transmission line;

each of said second sections having an average value of the wavelength
dispersion relatively smaller than said average value of the wavelength disper-
sion on the entire length of the optical fiber transmission line.

25 In the optical transmission system of the present invention, the transmis-
sion of the optical soliton pulses is controlled by controlling the wavelength
dispersion of the optical fiber transmission line for each long section includ-
ing a plurality of optical amplifier repeaters. In this case, the first sections
having an average value of the wavelength dispersion larger than the dispersion

value meeting with the soliton condition and the second sections having an average value of the wavelength dispersion smaller than the dispersion value meeting with the soliton condition are alternatively allocated in the optical fiber transmission line, so that the average value of the wavelength dispersion of the entire length of the optical fiber transmission line assumes a positive value.

Embodiments of the present invention will be described by way of example with reference to accompanying drawings, in which:

Fig. 1 is a connection diagram illustrating an optical fiber transmission line employed in an embodiment of the present invention;

Fig. 2 illustrates waveform diagrams explanatory of control operation of soliton pulses in an optical fiber transmission line of an embodiment of the present invention;

Figs. 3A and 3B are waveform diagrams illustrating optical pulse waveforms transmitted in the optical fiber transmission line of an embodiment of the present invention;

Fig. 4 is a connection diagram illustrating an embodiment of the present invention;

Fig. 5 is a characteristic diagram illustrating section wavelength dispersion values in the optical fiber transmission system according to an embodiment of the present invention; and

Fig. 6 illustrates waveform diagrams explanatory of

control operations of soliton pulses in a convention optical fiber transmission line.

5 With reference to Fig. 1, an optical transmission system of an embodiment of the present invention comprises an optical soliton transmission terminal station 1, an optical fiber 2, optical amplifier repeaters 3 for compensating for the loss of the optical fiber transmission line 2, and an optical soliton receiving terminal

station 4. The optical fiber 2 and the optical amplifiers 3 form an optical fiber communication line. The optical fiber transmission line 2 comprises first sections 6 each having a relatively larger wavelength dispersion value and second sections 5 each having a relatively smaller wavelength dispersion value.

5 Fig.2 shows variations ,in ordinate, of the wavelength dispersion value of the optical fiber, the optical pulse width and the peak power of the optical pulse ,while the abscissa is a distance on the optical fiber from the transmission terminal station.

The waveform of each transmitted optical pulse is a sech^2 waveform essential
 10 for the optical soliton transmission. The average value of the waveform dispersion for the entire optical transmission line is a positive value, which can be compensated for pulse compression caused by Kerr Effect (nonlinear optical effect) of the optical fiber. Moreover, the first sections each having a relatively larger wavelength dispersion value and the second sections each having
 15 a relatively smaller wavelength dispersion value are alternately allocated, so that the average value of the waveform dispersion for the entire optical transmission line is established to meet with the condition where the pulse width of the transmitted optical pulse and the regenerated output of each optical amplifier repeater meet with the optical soliton condition in a macro sense. In one
 20 of the second sections each having a relatively smaller wavelength dispersion value, the nonlinear optical effect is mainly effective so that the optical pulses are slightly compressed in a macro sense.

In each fiber section between two optical amplifier repeaters, optical pulses injected to fiber section are pulse-compressed at the begining of trans-
 25 mission by mainly effective nonlinear optical effect but the nonlinear optical effect is lowered due to light power attenuation as the optical pulses transmit through the fiber section, so the the optical pulses are expanding a little by main effect of waveform dispersion in place of pulse compression or monotonously compressed. In any case, the optical pulses transmit through the fiber

section under compression on an average. Therefore, the first section 6 having a larger wavelength dispersion value is connected. In this section 6, wavelength dispersion is mainly effective, so that pulse compression and pulse expansion are repeated in macro sense while the pulses are expanded in an average until the transmitted optical pulse is returned to the same pulse width as that of the injected optical pulse.

In the present invention, it is not necessary to restrictively control the wavelength dispersion value for each optical amplifier repeaters 3. Moreover, the length of the first section having a relatively larger wavelength dispersion value is not necessarily equal to the length of the second section having a relatively smaller wavelength dispersion value. Furthermore, allocation order of the first section and the second section can be optionally selected. As shown in Fig.3A, the pulse width (width of half maximum: about 40 ps) of a pulse transmitted through the first section having a relatively larger wavelength dispersion value is expanded a little in comparison with that of an injected optical pulse. Fig.3B shows a waveform of an optical pulse transmitted further through the second section having a relatively small wavelength dispersion value. The pulse width shown in Fig.3B is narrower than that shown in Fig.3A. It is understood that pulse control by average wavelength dispersion control can be performed in accordance with the present invention without strict wavelength dispersion control for each optical amplifier repeater in conventional dynamic soliton transmission.

With reference to Fig.4, an embodiment of the present invention comprises the optical soliton transmission terminal station 1, the optical fiber 2, the optical amplifier repeaters 3 and the optical soliton receiving terminal station 4. The optical fiber 2 and the optical amplifiers form an optical fiber communication liner. Short optical pulses of oscillation wavelength 1.558 microns transmitted from the optical transmission terminal station 1 is modulated by a pseudo-random pattern at a transmission rate of 5 Giga-bits/second.

the optical amplifier repeaters 3 are allocated to a span of about 33 kilometers. The output power of each one of the optical amplifier repeaters 3 is set to a value of -4 dBm with a transmitting pulse width of 35ps, while the average value of wavelength dispersion on the entire length 3000 kilometers of the optical fiber transmission line is set to a value of +0.4 ps/km/nm to meet substantially with the soliton transmission line comprises seventeen sections of different lengths, in which first sections having an average value of wavelength dispersion relatively larger than that of the entire length of the optical fiber transmission line and second sections having an average value of wavelength dispersion relatively smaller than that of the entire length of the optical fiber transmission line are alternately allocated.

Second lengths and the section average wavelength dispersion values are shown on Table 1, while a part thereof is illustrated in Fig.5.

Table 1

Section No.	Section Length(km)	Average Dispersion Value (ps/km/nm)
(1)	429	-0.043
(2)	33	+2.45
(3)	99	-0.37
(4)	66	+2.36
(5)	66	-0.86
(6)	66	+2.27
(7)	429	-0.076
(8)	66	+2.06
(9)	297	-0.068
(10)	33	+3.85
(11)	462	-0.043
(12)	33	+2.45
(13)	247	-0.079
(14)	33	+1.82
(15)	462	-0.037
(16)	33	+3.22
(17)	146	-0.003

Remarkable expansion or compression is not observed on received waveforms after transmitting through the optical fiber transmission line of 3000 kilometers, and good transmission performance, such as a low error rate less than 10^{-10} is achieved. It is therefore ascertained that optical soliton transmission can be stably accomplished in accordance with the present invention.

As mentioned above, stable optical soliton transmission is performed in this embodiment by controlling the wavelength dispersion value in view of an average of the wavelength dispersion value for a relatively long section, while the wavelength dispersion value is not controlled to be mutually equalized at the output of each one of the optical amplifier repeaters 3 as conventional dynamic soliton transmission.

In the present embodiment, the soliton transmission system has allocation order in which the second section having a relatively smaller average wavelength dispersion value and the first section having a relatively larger wavelength dispersion value are allocated in this order. However, this allocation order can be reversed.

The optical fiber transmission line can be formed by only a dispersion-shifted optical fiber having a zero-dispersion wavelength of about 1.55 microns or by including halfway conventional single-mode optical fiber (of zero dispersion wavelength: 1.3 microns) having a relatively larger wavelength dispersion.

The average wavelength dispersion value can be adjusted by inserting, in optical fiber or an amplifier repeater, dispersion media which is embodied to obtain a positive wavelength dispersion by the use of a conventional single-mode fiber etc.

As mentioned above, while high precision is required to each one of the optical amplifier repeaters and the optical fiber transmission line in the conventional dynamic soliton transmission because optical soliton pulses are controlled for each one of the optical amplifier repeaters in conventional technique. However, the system of the present invention is possible to

compensate for manufacturing deviation of the optical fiber by controlling the allocation of sections of the optical fibers since the optical soliton pulse transmission is controlled in a lump for a plurality of fiber sections.

Respective repeating sections of the wavelength dispersion values have more
5 freedom of the design so that a stable optical transmission system can be constructed in accordance with the present invention. Therefore, the optical communication system of the present invention has a wider allowance for deviations of the wavelength dispersion value of the optical fiber and has remarkable merits for realizing a practical optical soliton transmission
10 system.

CLAIMS

1. An optical communication system comprising :

an optical transmission terminal station for transmitting return-to-zero optical pulses including digital information;

an optical receiving terminal station for receiving the return-to-zero optical pulses;

an optical fiber connected across the optical transmission terminal station and the optical receiving terminal station; and

a plurality of optical amplifier repeaters inserted in the optical fiber for compensating for the loss of the optical fiber transmission line;

said optical fiber and said plurality of optical amplifier repeaters forming an optical fiber transmission line;

an average value of wavelength dispersion on the entire length of the optical fiber transmission line being a positive value capable of compensating for the pulse compression effect and the pulse expansion effect on the optical pulses applied to the optical receiving terminal station;

first sections and second sections being alternately allocated in the optical fiber transmission line;

each of said first sections having an average value of the wavelength dispersion relatively larger than said average value of the wavelength dispersion on the entire length of the optical fiber transmission line;

each of said second sections having an average value of the wavelength dispersion relatively smaller than said average value of the wavelength dispersion on the entire length of the optical fiber transmission line.

2. An optical communication system substantially as herein described with reference to the accompanying drawings.

Relevant Technical Fields

(i) UK Cl (Ed.M) H4B (BK18)

(ii) Int Cl (Ed.5) H04B 10/18

Databases (see below)

(i) UK Patent Office collections of GB, EP, WO and US patent specifications.

(ii)

Search Examiner
DR E PLUMMERDate of completion of Search
12 NOVEMBER 1993Documents considered relevant
following a search in respect of
Claims :-
ALL

Categories of documents

- X: Document indicating lack of novelty or of inventive step. P: Document published on or after the declared priority date but before the filing date of the present application.
- Y: Document indicating lack of inventive step if combined with one or more other documents of the same category. E: Patent document published on or after, but with priority date earlier than, the filing date of the present application.
- A: Document indicating technological background and/or state of the art. &: Member of the same patent family; corresponding document.

Category	Identity of document and relevant passages	Relevant to claim(s)
A	GB 2064161 A (WESTERN ELECTRIC)	
AP	EP 0554714 A1 (CORNING)	
AP	US 5185827 (ATT) & GB 2260048 A	

Databases: The UK Patent Office database comprises classified collections of GB, EP, WO and US patent specifications as outlined periodically in the Official Journal (Patents). The on-line databases considered for search are also listed periodically in the Official Journal (Patents).

This Page Blank (uspto)

**This Page is Inserted by IFW Indexing and Scanning
Operations and is not part of the Official Record**

BEST AVAILABLE IMAGES

Defective images within this document are accurate representations of the original documents submitted by the applicant.

Defects in the images include but are not limited to the items checked:

- ☐ **BLACK BORDERS**
- ☐ **IMAGE CUT OFF AT TOP, BOTTOM OR SIDES**
- ☐ **FADED TEXT OR DRAWING**
- ☐ **BLURRED OR ILLEGIBLE TEXT OR DRAWING**
- ☐ **SKEWED/SLANTED IMAGES**
- ☐ **COLOR OR BLACK AND WHITE PHOTOGRAPHS**
- ☐ **GRAY SCALE DOCUMENTS**
- ☐ **LINES OR MARKS ON ORIGINAL DOCUMENT**
- ☐ **REFERENCE(S) OR EXHIBIT(S) SUBMITTED ARE POOR QUALITY**
- ☐ **OTHER:** _____

IMAGES ARE BEST AVAILABLE COPY.

As rescanning these documents will not correct the image problems checked, please do not report these problems to the IFW Image Problem Mailbox.

This Page Blank (uspto)